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Regulatable spring-and-damper system in a vehicle

The invention relates to a regulatable spring-and-damper system in a vehicle according to the precharacterizing clause of claim 1 or 9.

In the publication DE 199 61 715 A1 there is a description of a spring-and-damper system which is fitted as a spring strut between the wheel and the body of a vehicle and is configured as a hydropneumatic system with a hydraulically filled displacer, a hydraulic accumulator and two lines connecting the displacer to the hydraulic accumulator. A regulatable throttle valve is arranged in one of the lines; the other line is surrounded by a device generating a magnetic field. The entire system is filled with a magnetorheological fluid, the flow properties of which can be changed by applying a magnetic field in one of the connecting lines. In this way, a variable damping force can be regulated in the line enclosed by the magnetic-field-generating device, whereas a constant damping force is generated in the parallel-running line with the throttle device. A spring force can be regulated in the system by means of the hydraulic accumulator, which has a compressible gas volume separated from the hydraulic medium.

An additional regulating possibility is provided by the supply or discharge of hydraulic medium via the throttle device. The volumetric flow of the hydraulic medium to be supplied or discharged represents a manipulated variable by means of which an actively controlled system can be realized. However, the supply of hydraulic fluid requires considerable expenditure of energy.

The invention is based on the problem of providing a regulatable spring-and-damper system which has properties that are essentially comparable to those of an active system but which only requires low expenditure of energy.

This problem is solved according to the invention by the features of claim 1 or 9. The subclaims specify expedient developments.

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The regulatable spring-and-damper system according to the invention in a vehicle comprises a passive spring element and a damping element which is mounted in parallel and is configured with a damping characteristic that can be regulated in a variable manner and is determined by comparison with a reference system that can be actively regulated. The spring-and-damper system represents a semi-active replacement system which is used instead of the active reference system and has essentially the same positive properties as the reference system but requires considerably less energy.

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The spring-and-damper system according to the invention comprises a software part and a hardware part, the software part representing an interface between a controller, for example for controlling a chassis, and the hardware part. The damping characteristic of the regulatable damping element can be continuously adapted in the course of operation to the current situation. Changing the damping characteristic allows generation of an overall force acting on the spring-and-damper system which is made up of a passive component - without open-loop or closed-loop control - and an active component. The current value of the damping characteristic thereby depends on a manipulated variable which would act on the final control element fitted in the equivalent, active reference system.

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Since, in the spring-and-damper system according to the invention, this manipulated variable is used solely for calculating the way in which the damping element is regulated, but need not be physically implemented in the spring-and-damper system, significant advantages in terms of energy and structural design are obtained, since no expenditure of energy has to be provided for the supply and discharge of the medium corresponding to the manipulated variable, and accordingly no structural device required for this has to be provided either. Rather, it is sufficient to influence the damping element of the system according to the invention by changing the damping characteristic. The laws governing the way in which the damping characteristic is to be regulated are based on a comparison of the mathematical behavior of the active reference system with that of the semi-active system.

Since the spring-and-damper system according to the invention has a behavior equivalent to that of the active reference system it is intended to replace, existing control strategies and approaches can be transferred directly to the system according to the invention. It is not absolutely necessary to develop new or adapted control strategies. In connection with the interface, the semi-active system has the same, or at least approximately the same, functionality as the corresponding active system.

The spring-and-damper system according to the invention merely comprises a passive spring element and a damping element which is mounted in parallel with the latter and has a damping characteristic that can be regulated in a variable manner, irrespective of the construction of the active spring-and-damper system to be replaced. Both mechanical and hydraulic, pneumatic or mixed systems come into consideration, both in respect of the active system to be replaced and in respect of the

semi-active spring-and-damper system actually used. The degree of complexity of the active system to be replaced is immaterial here; a different behavior on the part of the active system is taken into account via
5 the interface and the function calculated there for the damping characteristic, so that the semi-active spring-and-damper system can always have the same construction.

10 A hydropneumatic system with a displacer and a hydropneumatic spring accumulator as the spring element is advantageously used as the semi-active spring-and-damper system, the hydraulic damper communicating with the hydraulic side of the spring accumulator via a
15 connecting line in which a regulatable throttle is arranged. By changing the throttle cross section, the damping value can be changed.

To avoid low-frequency or quasi-steady components entering the calculation of the damping characteristic, the signal representing the manipulated variable can be subjected to high-pass filtering, in which frequencies in the signal above a predeterminable cutoff frequency are eliminated.

25 To repeat the essential idea of the invention in a general form: the regulatable spring-and-damper system according to the invention in a vehicle comprises a spring element and a damping element which is mounted
30 in parallel with it, one of the elements being configured in an adjustable manner. To realize a semi-active system, the spring element is passive and the damping element is configured with a damping characteristic that can be regulated in a variable
35 manner. The semi-active system can be described according to a force profile which can be represented as a function of a variable describing the spring constant of the passive spring element and/or of a

variable describing a damping value that can be regulated in a variable manner and/or of a variable describing a state variable of the system and/or of a variable describing the derivative with respect to time of the state variable. The damping element is regulated by the damping value following at least approximately a relationship which can be represented as a function of the variable describing the spring constant of the passive spring element and/or of a manipulated variable and/or of a variable describing the derivative with respect to time of the manipulated variable and/or of the variable describing the state variable of the system and/or of the variable describing the derivative with respect to time of the state variable. This relationship is based here on a function which is known from an actively regulatable reference system with an adjustable final control element. The force profile of the reference system can be described according to a relationship which can be represented as a function of the manipulated variable and/or of the variable describing the derivative with respect to time of the manipulated variable and/or of the variable describing the state variable of the system and/or of the variable describing the derivative with respect to time of the state variable, with the manipulated variable and/or the variable of the adjustable final control element describing the derivative with respect to time of the manipulated variable being determinable in a closed-loop and open-loop control unit according to a stored mathematical relationship. The spring-and-damper system represents a semi-active replacement system which is used instead of the active reference system and has essentially the same positive properties as the reference system but requires considerably less energy.

Further advantages and expedient configurations can be taken from the further claims, the description of the figures and the drawings, in which: /

5 Figure 1 shows a basic representation of an active reference system in a vehicle and also of a replacement system which can be used instead of the active system and comprises an interface and a semi-active spring-and-damper system,
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Figure 2 shows representations of an active reference system and of a semi-active spring-and-damper system, a spring element and a final control element being mounted in series and a damping element being mounted in parallel both with the spring element and with the final control element in the case of the active reference system, whereas the semi-active system comprises a passive spring element and a regulatable damping element mounted in parallel with it,
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Figure 3 shows a representation corresponding to Figure 2, the active reference system comprising a passive spring element and a passive damping element mounted in parallel with it and an active final control element mounted in series with both elements,
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Figure 4 shows an implementation for an active and a semi-active system corresponding to Figure 3 configured as a hydropneumatic spring strut,

35 Figure 5 shows a further exemplary embodiment of an active and a semi-active spring-and-damper system, an active subsystem being replaced by a semi-active subsystem.

In Figure 1, two spring-and-damper systems are represented: firstly, an active spring-and-damper system, which is referred to as the reference system 1 and in which an active, controlled regulation can be carried out as a function of state variables and manipulated variables of the system by means of a stored control strategy, and also a replacement system 2, which comprises an interface 3 and a semi-active spring-and-damper system 4. The replacement system 2 is intended to replace the active reference system 1, it being intended for the physical and mathematical properties of the reference system 1 also to be essentially realized in the semi-active replacement system 2. It is also intended that the replacement system 2 can be activated by the same control strategies as the reference system 1.

The transfer into the replacement system 2 of a manipulated variable u to be supplied, by means of which the active reference system 1 can be controlled, is carried out via the interface 3, in which the signals of the manipulated variable u are converted into a variable damping value d_u , which is regulated in the semi-active system 4 for regulating the damping characteristic in a variable manner. In this way, the active reference system 1 can be replicated by the replacement system 2. Entered by way of example in Figure 1 as the output variable is a force F_R for the reference system 1 and F_S for the semi-active system 4, these forces being identical or virtually identical in the case of an optimum transfer.

The reference system 1 represented in the left half of Figure 2, with an active spring-and-damper system, comprises a passive spring element 5 with the spring constant c , an active final control element 6 with the manipulated variable u , mounted in series with the

spring element 5, and a passive damping element 7 with the damping constant d , which is mounted in parallel both with the spring element 5 and with the final control element 6. The reference system 1 is configured as an active spring
5 strut, via which a vehicle wheel 8 of a vehicle is to be connected to the body of the vehicle. The force F_R acts on the reference system 1; z denotes the travel of the spring strut, which represents the state variable of the system.

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The active reference system 1 is replaced by the semi-active replacement system 2. The replacement system 2 comprises a passive spring element 5 and an active
15 damping element 9, which is mounted in parallel with it and the damping value d_u of which can be regulated to change the damping characteristic of the damping element. The replacement system 2 is also configured as a spring strut on which the force F_S acts. The travel is likewise denoted by z ; it also assumes the function
20 of a state variable in the replacement system 2.

The force F_R acting on the reference system 1 can be described in a general way according to the relationship

$$F_R = -f(z, \dot{z}, u, \dot{u})$$

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as a function f of the state variable z , of the derivative with respect to time \dot{z} of the state variable, of the manipulated variable u and of the derivative with respect to time \dot{u} of the manipulated
30 variable.

The force F_S acting on the replacement system 2 can be described in the case of the implementation of the replacement system 2 that is represented in Figure 2 by
35 the relationships

$$F_S = -c \cdot z - d_u \cdot \dot{z}$$

$$d_u = \frac{-c \cdot z + f(z, \dot{z}, u, \dot{u})}{\dot{z}}$$

where c is the spring constant of the passive spring element 5 (identical to the spring constant or the spring element 5 of the reference system 1), d_u is the variable damping value of the regulatable damping element 6 and $f(z, \dot{z}, u, \dot{u})$ denotes the function known from the reference system 1.

To avoid the damping value d_u tending toward infinity when there is a zero crossing of the derivative with respect to time \dot{z} of the state variable, an approximation function is introduced for the damping value d_u :

$$d_u \approx \frac{\dot{z}}{\lim_{\dot{z}^2 \rightarrow v} [\dot{z}^2]} \{ -c \cdot z + f(z, \dot{z}, u, \dot{u}) \} .$$

In this, $\lim_{\dot{z}^2 \rightarrow v} [\dot{z}^2]$ denotes the permissible interval within which the square of the rate of the state variable may move, a limit value v , which is for example $\left(0.001 \frac{m}{s}\right)^2$, being prescribed as the lower permissible limit, whereas the interval is open in the upward direction. The manipulated variable u or the derivative with respect to time \dot{u} of the manipulated variable is determined in a closed-loop and open-loop control unit in accordance with a stored control or calculation specification.

In order to ensure that low-frequency and quasi-steady components do not enter the conversion for the damping adjustment of the replacement system, the manipulated variable u can be subjected in the closed-loop and open-loop control unit to a high-pass filtering according to the relationship

$$u_{HP} = \frac{T_{HP} \cdot \dot{u}}{T_{HP} \cdot \dot{u} + u}$$

where T_{HP} denotes a gain factor according to the relationship

$$T_{HP} = \frac{1}{2 \cdot \pi \cdot f_{HP}}$$

f_{HP} denotes the cutoff frequency of the high-pass filtering. The high-pass-filtered manipulated variable u_{HP} is included in the determination of the damping value d_u .

In the case of the example according to Figure 2, the force F_R acting on the reference system 1 is calculated according to the relationship

$$F_R = -f = -d \cdot \dot{z} - c(z - u) .$$

The variable damping value d_u is hereby obtained as

$$d_u = \frac{-c \cdot z + f}{\dot{z}} = d - \frac{c \cdot u}{\dot{z}}$$

or, by applying the approximation function, as

$$d_u \approx d - \frac{c \cdot u \cdot \dot{z}}{\text{limit}[\dot{z}^2]_u^\infty} .$$

In the case of the exemplary embodiment according to Figure 3, the actively regulatable reference system 1 comprises a passive spring element 5 with the spring constant c , a passive damping element 7 with the damping constant d mounted in parallel with the passive spring element and a final control element 6 with the manipulated variable u mounted in series with both elements. The function f of the reference system can be described according to the relationship

$$f = d(\dot{z} - \dot{u}) + c(z - u)$$

where the derivative with respect to time \dot{u} of the manipulated variable is now also included in this relationship. This produces the regulatable damping value d_u of the damping element 9 of the replacement system 2 as

$$d_u = \frac{-c \cdot z + f}{\dot{z}} = d - \frac{d \cdot \dot{u} + c \cdot u}{\dot{z}}$$

or, as an approximation function, as

$$d_u \approx d - \frac{(d \cdot \dot{u} + c \cdot u) \dot{z}}{\lim_{\dot{z} \rightarrow 0} [\dot{z}^2]_v}$$

In Figure 4, a hydropneumatic spring strut in a vehicle
 5 is represented as the spring-and-damper system and has
 in principle the same construction as the system from
 Figure 3. The active hydropneumatic reference system 1
 shown in the left half of the figure has a hydraulic
 final control element 6, which can be regulated by
 10 means of a volumetric flow of oil Q_{AHP} that can be
 supplied or discharged, whereby the force F_R can be
 regulated. The volumetric flow of oil Q_{AHP} is
 proportional to the first derivative \dot{u} of the
 manipulated variable:

$$\dot{u} = \frac{Q_{AHP}}{A_{HK}},$$

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where A_{HK} denotes the surface area of the main chamber
 of the final control element 6 configured as a
 displacer. For the manipulated variable u there is the
 relationship:

$$u = \frac{1}{A_{HK}} \int Q_{AHP} dt$$

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The hydraulic chamber of the final control element 6
 communicates via a line 11, in which a passive damping
 element 7 configured as a constant throttle is
 arranged, with the likewise passively configured spring
 25 element 5, which is configured as a hydropneumatic
 spring accumulator and has a pneumatic chamber with the
 volume V_{FS} and the gas or spring accumulator pressure
 p_{FS} prevailing in it. The hydropneumatic spring element
 5 permits vertical springing of the spring strut; the
 30 constant throttle 7 with the damping constant d
 generates a damping force proportional to the
 volumetric flow Q_D through the throttle. The force F_R

acting on the reference system 1 is described by the equation

$$F_R = -f = d \left(\dot{z} + \frac{1}{A_{HK}} Q_{AHP} \right) + c \left(z + \frac{1}{A_{HK}} \int Q_{AHP} dt \right)$$

In the case of the replacement system represented in the right half of Figure 4, a volumetric flow of oil is not introduced into the system or discharged, but only redirected between the components of the system. A passive displacer 10, on which the vehicle wheel 8 is fitted, is provided. Arranged in the line 11 between the displacer 10 and the hydropneumatic spring element 5 is the damping element 9, which is configured as an adjustable throttle and has the regulatable damping value d_u , which can be regulated by means of a suitable adjusting unit, which acts on the throttle, by equating the relationship given above for the force F_R in the reference system 1 and the force F_S in the semi-active replacement system 2 according to the relationship

$$d_u \approx d + \frac{\dot{z}}{\lim_{\dot{z}^2 \rightarrow \infty}} \left(d \frac{1}{A_{HK}} Q_{AHP} + c \frac{1}{A_{AH}} \int Q_{AHP} dt \right)$$

The spring stiffness c of the hydropneumatic spring element 5 can be calculated with a known reference pressure p_0 and a known spring stiffness c_0 at this reference pressure as a function of the pressure p_{FS} in the gas accumulator of the spring element 5 and of the isentropic exponent k of the gas in the gas accumulator according to the relationship

$$c = \left(\frac{p_{FS}}{p_0} \right)^{\frac{k+1}{k}} c_0$$

In the case of the exemplary embodiment according to Figure 5, both the actively regulatable reference system 1 and the semi-active replacement system 2 are respectively configured as a subsystem within an overall system, each subsystem being mounted in parallel with an additional, passive spring element 12 with the spring constant c_2 . The subsystem of the

reference system 1 is identical to that of the exemplary embodiment from Figure 3; accordingly, the function f of the reference subsystem can be described according to the relationship

$$f = d(\dot{z} - \dot{u}) + c_1(z - u)$$

where c_1 denotes the spring constant of the passive spring element 5 within the reference subsystem 1. The damping value d_u of the damping element 9 in the replacement subsystem 2 is hereby obtained as

$$d_u = d - \frac{d \cdot \dot{u} + c_1 \cdot u}{\dot{z}} \approx d - \frac{(d \cdot \dot{u} + c_1 \cdot u) \dot{z}}{\lim_{\dot{z} \rightarrow \infty} [\dot{z}^2]}$$

Referred to the overall system, the overall force F_G of the reference system can be given as

$$F_G = -d(\dot{z} - \dot{u}) - c_1(z - u) - c_2 \cdot z$$

and of the replacement system as

$$F_G = -d_u \cdot \dot{z} - (c_1 + c_2)z = -d_u \cdot \dot{z} - c^* \cdot z$$

where c^* denotes a replacement stiffness for the overall replacement system.